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# Modified Melt-Blown Nonwovens for Respiratory Protective Devices Against Nanoparticles

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Division of Molecular Engineering.

## Abstract

Epidemiological studies of the effect of harmful nanoparticles on the human body prove that efficient protective measures need to be developed. This applies, in particular, to respiratory protection equipment in which filtration nonwovens are the essential structural material. This paper discusses a method for improving the efficiency of electret filtration nonwovens for nanoparticles by using polypropylene (PP) admixed with additives with varying electrostatic potentials. The investigation was carried out using amber (negative charge) and perlite beads (positive charge) incorporated into the polymer stream using melt-blown technology. Filtration efficiency was evaluated using standard methods with paraffin oil mist and sodium chloride aerosol and non-standard methods with nanoparticles. The studies proved that strengthened electrostatic interaction effects owing to the modifiers provide a promising method for improving the efficiency of electret nonwovens against nanoparticles.

**Key words:** filtration, efficiency, polypropylene nonwoven, melt-blown, modification, corona treatment, nanoparticles.

regard to gaining acceptance from users). Methods which generate or enhance electrostatic attraction forces between fibres and aerosol particles captured from the flowing air stream are commonly used to improve the filtration efficiency of such materials. Studies [6 – 11] have demonstrated that fibre electrostatic activation considerably improves filtration efficiency without any increase in air resistance. Corona discharge technology is widely used in the manufacture of melt-blown filtration materials for the manufacture of respiratory protective devices, involving a potential difference generated between an electrode and counter electrode, which is sometimes the surface of the receiving device. Due to its good processability and low cost, (PP) is the fibre-forming raw material used for the manufacture of such fibres employed in respiratory protective devices. However, considering its electrostatic properties and, in particular, the persistence of the electret effect, PP is

frequently considered suboptimal when used to protect against harmful nanoparticles. This work therefore discusses technological experiments conducted to determine how PP electret melt-blown nonwovens should be modified. Our objective was to develop a method for improving the efficiency of melt-blown PP electret filtration nonwovens for nanoparticles using modifiers with varying electrostatic potentials.

## Experimental materials

MOPLEN HP 456 J grade isotactic polypropylene (PP) with a melt index (MLI) of 3.4 g/10 min (manufacturer: Lyondell-Basell, Germany) was the raw material for the filtration nonwovens.

## Modifiers

Two granulates were used in the modification process:

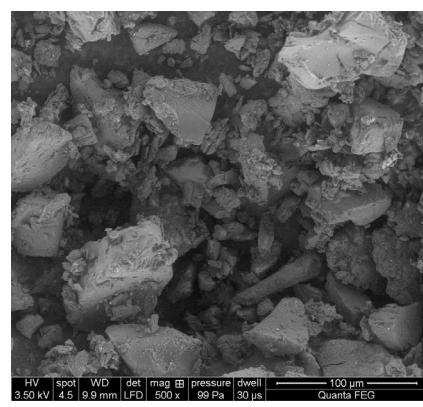


Figure 1. SEM image of amber granulate surface.

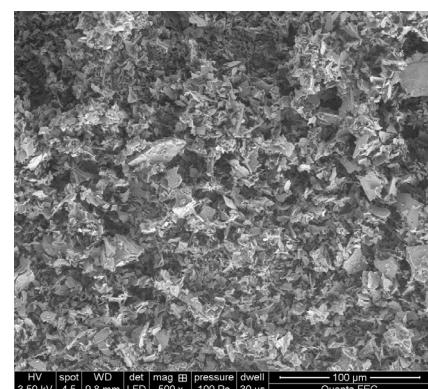


Figure 2. SEM image of perlite granulate surface.

- natural resin (amber) with a negative potential (supplier: EDAN, Poland),
- volcanic rock (perlite) with a positive potential (manufacturer: TERMOFOR-BEŁCHATÓW, Poland).

To obtain the desired electrostatic effect, the modifiers were selected to occupy different positions in the triboelectric series, gathering a positive or negative electrostatic charge. They are also good insulators to prevent charge release.

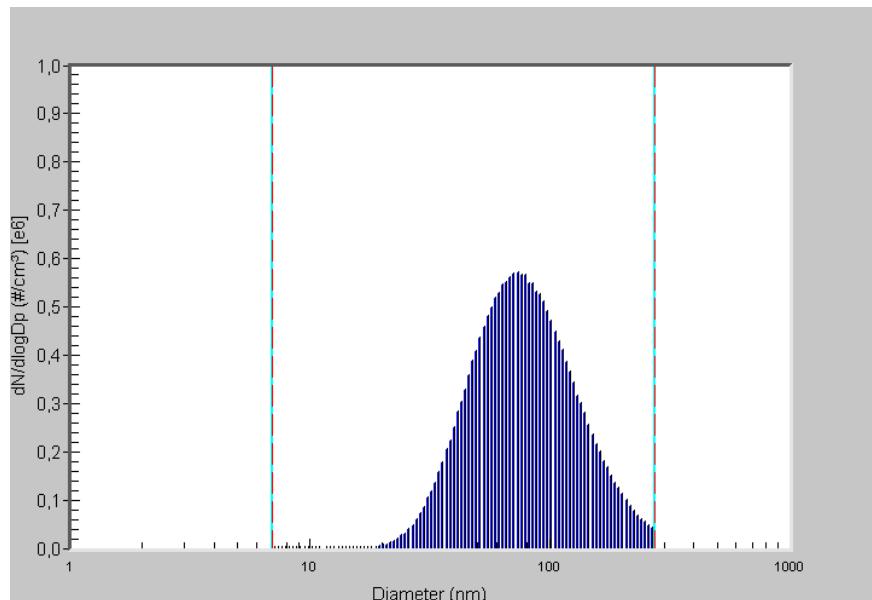
A Quanta F 200 scanning electron microscope (500 x magnification) was used to determine the shape and bead size of the modifiers. In the case of amber the size of particles was in the range of 2-80 µm and for perlite the size range was from 0.2 to 10 µm. The differences are illustrated in **Figures 1** and **2**. The shape and size of the NaCl aerosol nanoparticle are illustrated in **Figure 4**.

#### Processing equipment

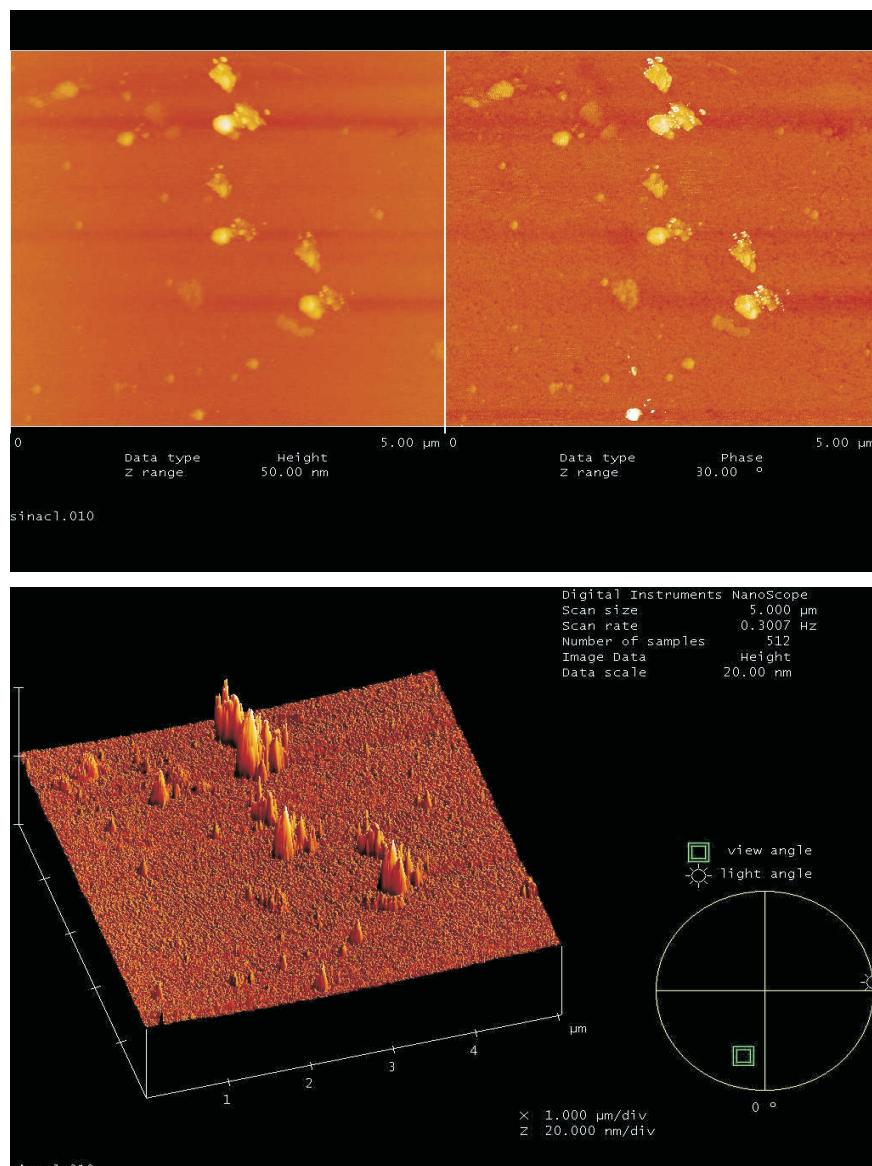
The technological research was performed at the experimental site of the Central Institute for Labour Protection – National Research Institute (CIOP-PIB), which is discussed in detail in [12].

The PP polymer (beads) was fed from the charging hopper into a heated extruder cylinder. Before extrusion from the fibre-forming head, it was brought to appropriate viscosity. Compressed air was pumped from the regulator to a heater, in which it was dried and heated to the appropriate temperature. Subsequently it was sent to the fibre-forming head, and at the outlet it blew polymer streams forced through nozzles into elementary fibres. They were deposited on the receiver and formed a compact porous fleece (nonwoven). The nonwoven production unit has adjustment points to change manufacturing parameters. The parameters listed in **Table 1** were used when moulding PP nonwovens with and without a modifier. **Table 2** shows characteristics of the structural parameters of the resulting PP nonwovens with and without a modifier.

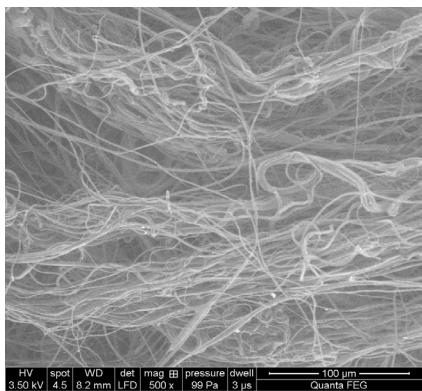
Modifiers in the form of beads were added at the fibre formation stage (5% by weight of PP) according to the patent [13]. There is a detailed description in [12]. **Figures 6 and 7** show the distribution of the modifiers in the filtration nonwoven. For comparison, **Figure 5** shows the PP nonwoven without a modifier.



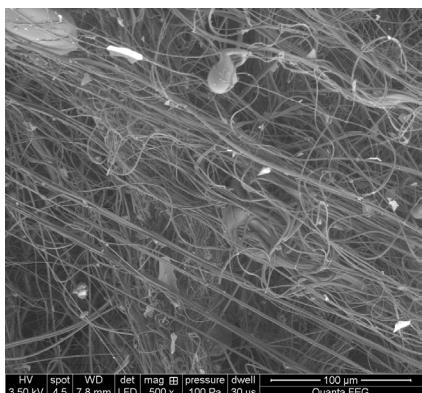
**Figure 3.** Size distribution of NaCl nanoaerosol.



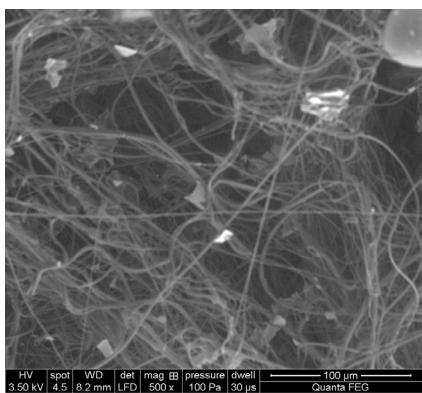
**Figure 4.** NaCl aerosol nanoparticles: A) 2D view; B) 3D view.



**Figure 5.** SEM image of (PP) nonwoven without a modifier.



**Figure 6.** SEM image of amber-modified (PP) nonwoven.



**Figure 7.** SEM image of perlite-modified (PP) nonwoven.

The nonwoven structural parameters with and without a modifier are shown as a pore fractional distribution (**Table 3**) due to the major impact of the parameter on filtration efficiency for aerosol particles [14].

A device for discharge emission was used to confer electret properties to the nonwoven with and without a modifier. It has a tip electrode at the receiving device, to which positive voltage is connected, and a counter electrode under the grid which collects nonwoven fleece, to which

negative voltage is connected. The total charging voltage is 30 kV, which generates current in the range of  $300 \pm 50 \mu\text{A}$ . The system ensures control of the flow of non-dissipated charges.

## ■ Testing methods

The efficiency of the filtration materials was established by measuring the number of particles that were not blocked by these materials, described as particle penetration. Particle-penetration and air-resistance (respiratory resistance) tests were carried out using standard methods for the evaluation of respiratory protection equipment specified in the standards [15, 16] and using a non-standard method discussed below. Two model aerosols were used in the standard tests: sodium chloride and paraffin oil mist.

Sodium chloride (NaCl) in suspension, generated from a 0.1% aqueous solution using a collision nebulizer, was used for nanoparticle penetration testing. Nanoaerosol was fed through a drier and ionisation neutralizer into a chamber with a nonwoven sample tested. **Figure 3** shows the size distribution of the nanoaerosol used. The graf was obtained with the use of a TSI condensation particle counter connected to an electrostatic classifier.

The NaCl nanoparticles used in the testing were cubic, with the fractal dimension being similar (3). They were neutralised by an ionisation neutraliser, with a dielectric constant of 5.9. Tests of nanoparticle penetration through the filtration nonwovens were performed using a TSI 3080 electrostatic classifier and a TSI 3775 condensation particle counter. The measurement range of the system ensures a testing range of between 7 nm and 270 nm, divided into 90 measurement grades. The duration of the tests was set at 7 minutes to enable calculation of the average penetration value for three cycles of 126 s each, including 15 s breaks between measurement cycles to calculate the average value of penetration

**Table 1.** Technological parameters of melt-blown production.

Process technological parameters	PP
Temperature, extruder zone 1, °C	280
Temperature, extruder zone 2, °C	270
Air temperature, °C	300
Nozzle temperature, °C	294
Air flow rate, m <sup>3</sup> /h	8
Polymer flow rate, g/min	24
Nozzles to collector distance, cm	16
Collector speed, m/s	0.00317
Supply voltage for fibre-forming head-heating elements, V	162

**Table 2.** Structural parameters of PP nonwovens without a modifier.

Basis weight, g/m <sup>2</sup>	90 ± 5
Thickness of non-woven, mm	2.12
Min fibre diameter, µm	0.27
Max fibre diameter, µm	2.08
Mean fibre diameter, µm	0.74
Standard deviation, µm	0.323

for the three cycles of 126 s each (including a 15 s break between the measured cycles to reset the electrostatic particle classifier). The tests were carried out at a volume value of aerosol flow intensity of 5400 l/h. The surface of the sample tested was constant for all measurements and was set at 0.01 m<sup>2</sup>. The environmental conditions during the tests were as follows: surrounding temperature  $20 \pm 5^\circ\text{C}$  and relative air humidity  $50 \pm 20\%$ .

A diagram of the measuring site is shown in **Figure 8**.

The measurement results were evaluated statistically. This included:

- determination of mean values, variance and standard deviations for NaCl nanoparticle penetration, size: 50 – 275 nm,
- normal distribution tests for the results: Shapiro-Wilk test,
- variance tests (Fisher-Snedecor test) and mean tests (Student t test for equal variance values or Cochran-Cox test for different variance values depending on the results of the Fisher-Snedecor test) between paired samples.

**Table 3.** Pore fractional distribution in melt-blown nonwovens without electrostatic charge.

Nonwoven type	Equivalent diameter of the largest pores, µm	Main pore fraction, µm	Mean value for the main pore fraction, µm
Polypropylene nonwoven without-modifier	47.36	11.90 – 14.70	12.9
Perlite - modified polypropylene nonwoven	39.26	10.95 – 13.43	11.7
Amber - modified polypropylene nonwoven	37.83	9.23 – 11.63	9.7

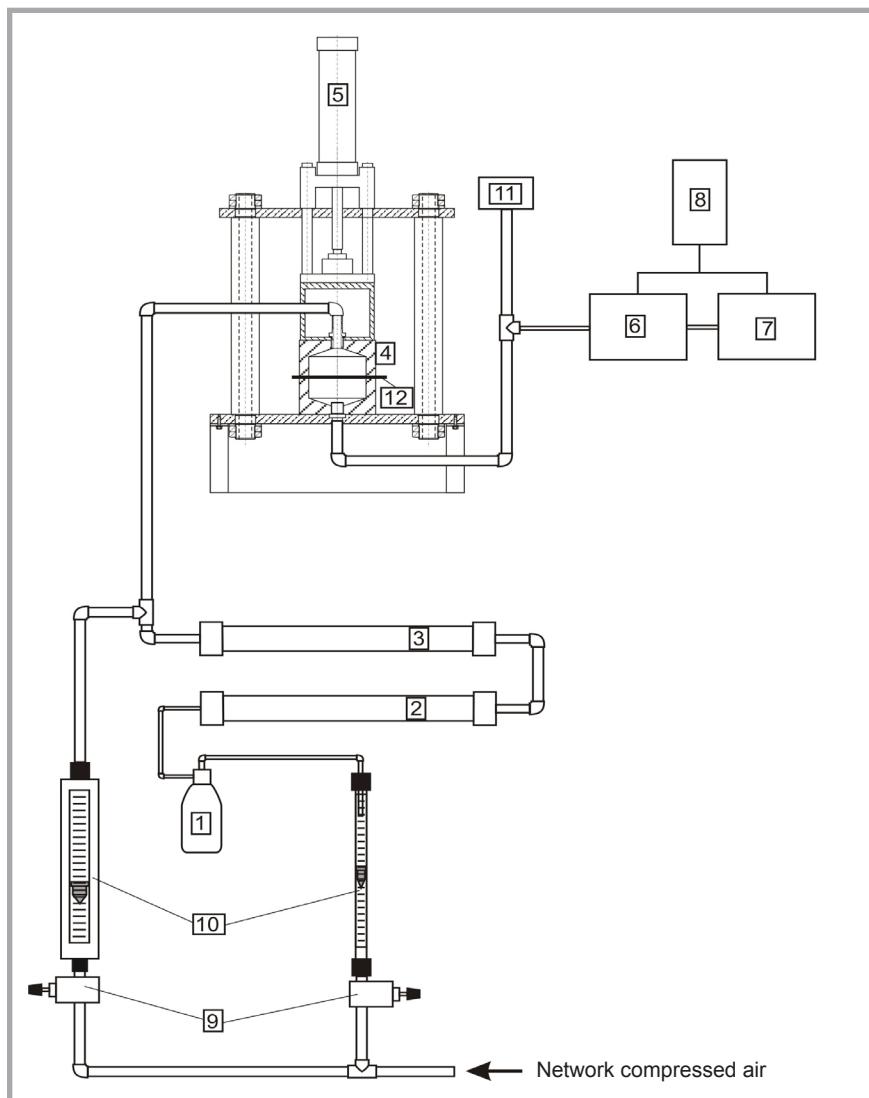
## Results and analysis

**Table 4** shows the results of penetration tests for standard aerosol particles: sodium chloride (mean particle diameter: 0.5 µm) and paraffin oil mist (mean particle diameter: 0.3 µm) determined using commonly used methods for the evaluation and classification of the efficiency of respiratory protection equipment against harmful aerosols (dust, fumes, mist) according to European Standard EN 13274-7:2008 [15].

The plots (**Figure 9** see page 110) show the results of NaCl nanoparticle penetration through nonwovens with and without modifiers, divided into nanoparticle size grades, and **Table 5** shows mean values for the particles in the range of 50 nm to 275 nm.

The results shown in **Table 4** confirm that corona discharge used when moulding fibres using melt-blown technology leads to the improved efficiency of pollutant-particle capture from the air stream. The reduced number of particles penetrating through electret filtration nonwovens compared to non-electret varieties is similar (statistically insignificant difference) in all of the varieties tested before and after modification. Because two particle types were used in standard tests: solid, represented by NaCl, and liquid, represented by paraffin oil mist, differences occurred between aerosol penetration values for the same nonwoven varieties. This results from particle size differences for both aerosol types and electrostatic properties, which lead to the prevalence of distinct liquid (mist) and solid (dust) particle deposition mechanisms on fibres. It was noted that adding modifiers (perlite and amber) with different electric potentials did not lead to an increase in non-electret nonwoven efficiency compared to non-modified nonwovens. This is primarily due to the fact that filtration efficiency in the aerosol particle size range of 0.3 µm to 0.5 µm is strongly dependent on nonwoven porosity, which is similar for all of the nonwovens tested (**Table 3**).

Distinct results were seen for NaCl nanoparticle penetration. **Figure 9** show the relationship between penetration and nanoparticle size for varieties modified by amber and perlite beads. For non-electret nonwovens, the modifiers did not lead to any significant changes in the efficiency of nanoparticle deposition on PP fibres. Mechanical attraction forces, whose ef-



**Figure 8.** Schematic diagram of the experimental set up; 1 – Nanoaerosol generator, 2 – Desiccant, 3 – Electrostatic charge neutraliser, 4 – Testing chamber, 5 – Sample holder, 6 – Electrostatic particle classifier, 7 – Condensation nanoparticle counter, 8 – Personal computer, 9 – Compressed air valve, 10 – Flowmeter, 11 – High efficiency filter, 12 – Test sample.

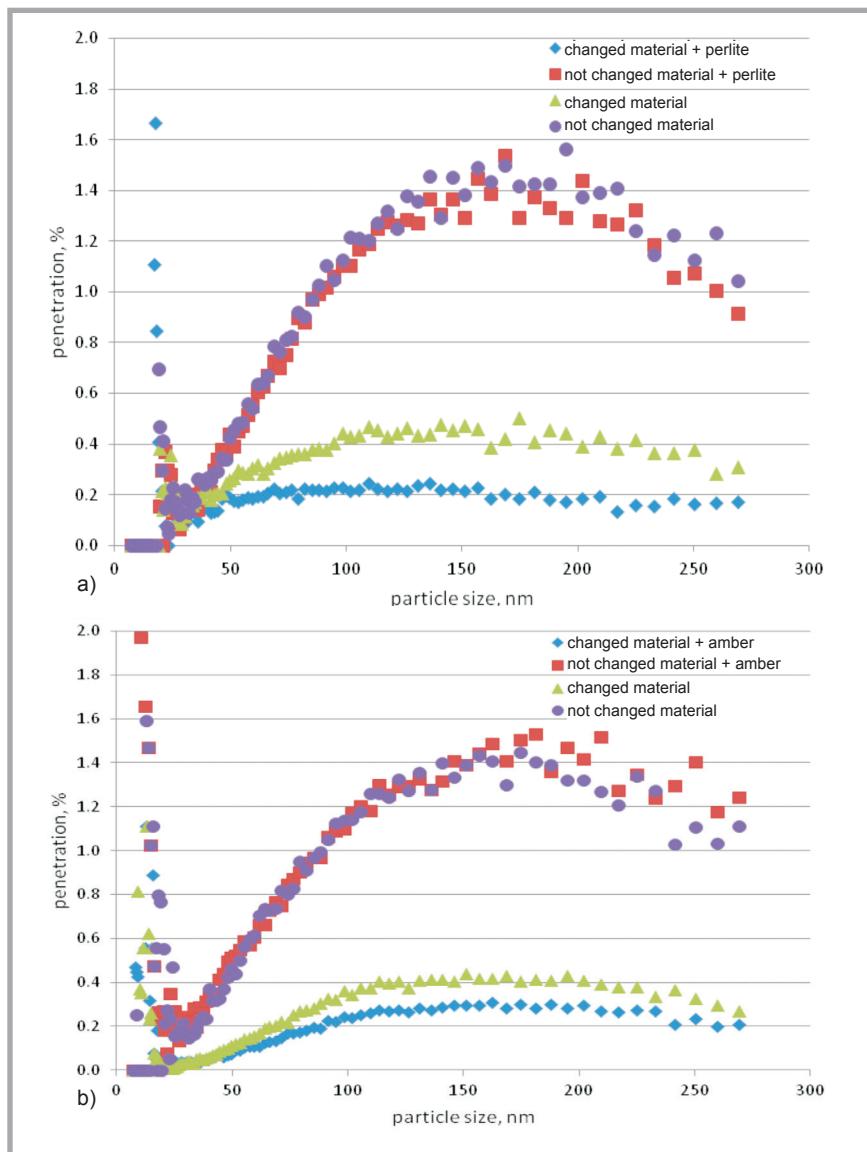
ficiency is largely determined by pore size, were the prevalent mechanism of nanoparticle deposition. However, when modifiers were incorporated in the electret nonwovens, the expected efficiency improvement was seen as compared to

unmodified non-electret nonwovens. This effect depends on nanoparticle size, and is strongest between 50 and 200 nm.

As the filtration respiratory protection equipment was evaluated using standard

**Table 4.** Nonwoven filtration parameters determined by standard methods [15, 16].

Nonwoven type	Mean sodium chloride aerosol penetration, %	Mean paraffin oil mist aerosol penetration, %	Mean air resistance, Pa
Polypropylene nonwoven, charged	0.78	2.89	270
Polypropylene nonwoven, uncharged	5.46	5.75	260
Perlite-modified polypropylene nonwoven, charged	0.44	1.35	290
Perlite-modified polypropylene nonwoven, uncharged	3.35	3.86	275
Amber-modified polypropylene nonwoven, charged	0.51	1.82	255
Amber-modified polypropylene nonwoven, uncharged	3.75	5.14	250



**Figure 9.** Results of NaCl nanoparticle penetration through electret nonwovens with and without a modifier in the form of amber (a) and perlite (b) beads.

methods with reference to the defined mean particle size typical of an aerosol type, the mean penetration index for nanoparticles was also determined (**Table 5**). It follows from these values that the perlite-modified electret nonwoven (positive charge) is the most favourable, having the lowest nanoparticle penetration index. This is also confirmed in the plot of the relationship between penetration values and nanoparticle sizes (**Figure 9.b**).

A statistical evaluation was performed to determine the significance of differences in the nanoparticle penetration index for the nonwoven varieties prepared. The results are shown in a matrix (**Table 6**). The statistical tests were performed at the significance level  $\alpha = 0.05$ .

The results of the statistical analysis confirmed our earlier assumptions related to improving the efficiency of electret

filtration nonwovens for nanoparticles by means of modifiers added to PP. Irrespective of the type of modifier used, all of the varieties of the melt-blown nonwovens had air resistance (breathing resistance) at a level of 250 Pa to 290 Pa (**Table 4**). This confirms that the modification method used for melt-blown nonwovens improved particle retention efficiency in the filtration material without significantly increasing breathing difficulties for equipment users. Furthermore it was noted that the values are similar to those commonly achieved by respiratory protective devices.

## Conclusions

We have proved that it is possible to modify PP electret melt-blown nonwovens to improve their filtration efficiency (lower number of particles penetrating through filtration nonwovens) by adding modifiers with various electrostatic potentials to the polymer material. A greater improvement in electret filtration efficiency was seen for nonwoven modification with perlite beads (positive) and positive corona discharge than for amber beads (negative) and positive corona discharge. When the modifiers used in PP nonwovens had the same sign as the corona discharge, their electrostatic potential increased.

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**Table 5.** Mean NaCl nanoparticle penetration through the nonwovens with and without a modifier.

	Amber-modified polypropylene nonwoven		Perlite-modified polypropylene nonwoven		Polypropylene nonwoven	
	with electrostatic charges	without electrostatic charges	with electrostatic charges	without electrostatic charges	with electrostatic charges	without electrostatic charges
<b>mean</b>	2.396	12.293	1.934	11.271	3.664	11.768
<b>standard deviation</b>	0.253	3.059	0.679	3.025	0.774	2.971
<b>variance</b>	0.064	9.355	0.461	9.153	0.600	8.826

**Table 6.** List of statistical test results; + Statistically significant differences (mean A ≠ mean B), - No statistically significant differences (mean A = mean B).

B		A		Amber-modified polypropylene nonwoven		Perlite-modified polypropylene nonwoven		Polypropylene nonwoven	
		with electrostatic charges	without electrostatic charges	with electrostatic charges	without electrostatic charges	with electrostatic charges	without electrostatic charges	with electrostatic charges	without electrostatic charges
Amber-modified polypropylene nonwoven	with electrostatic charges		+	+	+	+	+	+	+
	without electrostatic charges	+		+	-	+	+	+	-
Perlite-modified polypropylene nonwoven	with electrostatic charges	+	+		+	+	+	+	+
	without electrostatic charges	+	-	+		+	+	+	-
Polypropylene nonwoven	with electrostatic charges	+	+	+	+				+
	without electrostatic charges	+	-	+	-	+		+	

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